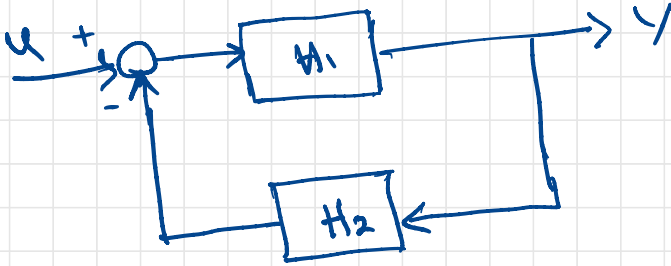


Absolute stability:



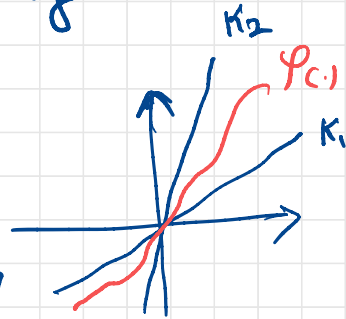
- Passivity theorem:

if H_1 and H_2 are passive, then the FB sys. is passive \Rightarrow stable closed loop

- We study the special case where H_1 is linear and H_2 is a sector nonlinearity

$$H_1: \begin{cases} \dot{x} = Ax + Bu \\ y = Cx + Du \end{cases}$$

$$H_2: y = \varphi(u), \varphi \in [K_1, K_2]$$



- Problem: find conditions for H_1 s.t. the FB sys. is stable.

- We use passivity to answer this question.

Passivity for linear systems:

$$\dot{x} = Ax + Bu$$

$$y = Cx + Du$$

$$\Leftrightarrow \hat{y}(s) = G(s)\hat{u}(s)$$

transfer function

- $x \in \mathbb{R}^n, y, u \in \mathbb{R}^p$

- To discuss passivity for lin. sys. we need to introduce the notion of positive real transfer functions.

Def:

- When $p=1$ (SISO), $G(s)$ is positive real if

1) all poles are in LHP ($\operatorname{Re}(s) < 0$)

2) $\operatorname{Re}(G(j\omega)) \geq 0 \quad \forall \omega$ st. $j\omega$ is not a pole

Nyquist plot is in right-hand plane.

3) if $j\omega$ is a pole, then it is a simple pole

and $\lim_{s \rightarrow j\omega} (s-j\omega)G(s) \geq 0$

- $G(s)$ is strictly positive real if $G(s-\varepsilon)$ is positive real for some $\varepsilon > 0$

- The definition can be extended to MIMO
(see Def 6.4)

Examples:

a) $G(s) = \frac{1}{s} \rightsquigarrow$ only pole $s=0$

\Rightarrow 1) all poles in LHP \checkmark

2) $\operatorname{Re}(G(j\omega)) = \operatorname{Re}\left(\frac{1}{j\omega}\right) = 0 \checkmark$

3) $\lim_{s \rightarrow 0} sG(s) = 1 \geq 0 \checkmark$

\Rightarrow positive real

but not strictly positive real because

$G(s-\varepsilon) = \frac{1}{s-\varepsilon}$ has pole $s=\varepsilon > 0$

$$b) \quad G(s) = \frac{1}{s+a} \quad \text{for } a > 0$$

this is positive real

1) pole $s = -a$ in LHS ✓

$$2) \quad \operatorname{Re}(G(j\omega)) = \operatorname{Re}\left(\frac{1}{j\omega+a}\right) = \frac{a}{a^2+\omega^2} \geq 0$$

No imaginary pole

Also, strictly positive real because

for $\varepsilon = a > 0$, $G(s-a) = \frac{1}{s}$ is positive real.

$$c) \quad G(s) = \frac{1}{s^2+s+1}$$

when $|\omega| > 1$

$$G(j\omega) = \frac{1}{j\omega+1-\omega^2} \Rightarrow \operatorname{Re}(G(j\omega)) = \frac{1-\omega^2}{(1-\omega)^2+\omega^2} < 0$$

\Rightarrow not positive real.

- In general, if $G(s) = \frac{P(s)}{Q(s)}$ is positive real

then relative degree = $\deg(Q) - \deg(P) \leq 0$ or 1

Positive real lemma: (Lemma 6.2, 6.3)

- Assume (A, B) is controllable and (A, C) is observable
- Transfer function $G(s) = C[sI - A]^{-1}B + D$ is positive real iff \exists a p.d. matrix P and matrices L, W , s.t.

$$PA + A^T P = -L^T L$$

$$PB = C^T - L^T W$$

$$W^T W = D + D^T$$

$$\Leftrightarrow \underbrace{\begin{bmatrix} PA + A^T P & PB - C^T \\ B^T P - C & D + D^T \end{bmatrix}}_{= - \begin{bmatrix} L^T \\ W^T \end{bmatrix} [L, W]} \preceq 0$$

- Strictly positive real if for some $\varepsilon > 0$

$$PA + A^T P = -L^T L - \varepsilon P$$

$$PB = C^T - L^T W$$

$$W^T W = D + D^T$$

Lemma 6.4:

(strict) positive real \iff (strict) passivity

proof:

- Consider $V = \frac{1}{2} x^T P x$, where P is from positive real lemma.

$$\dot{V} = \frac{1}{2} x^T (PA + A^T P) x + x^T P B u$$

$$\begin{aligned} PA + A^T P &= -L^T L \\ PB &= e^T L^T W \end{aligned}$$

$$= -\frac{1}{2} x^T L^T L x + x^T C^T u - x^T L^T W u$$

$$= -\frac{1}{2} (Lx + Wu)^T (Lx + Wu)$$

$$+ \frac{1}{2} u^T W^T W u + x^T e^T u$$

$$\begin{aligned} W^T W &= D + D^T \\ Cx &= y - Du \end{aligned}$$

$$\leq \frac{1}{2} u^T (D + D^T) u + y^T u - \cancel{u^T D^T u}$$

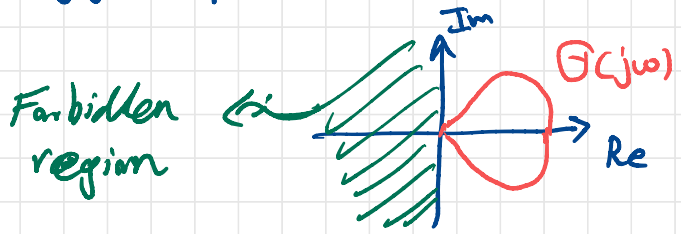
$$= y^T u \implies \text{passive}$$

- The proof for strict passivity is similar

$$\dot{V} \leq y^T u - \frac{\epsilon}{2} x^T P x$$

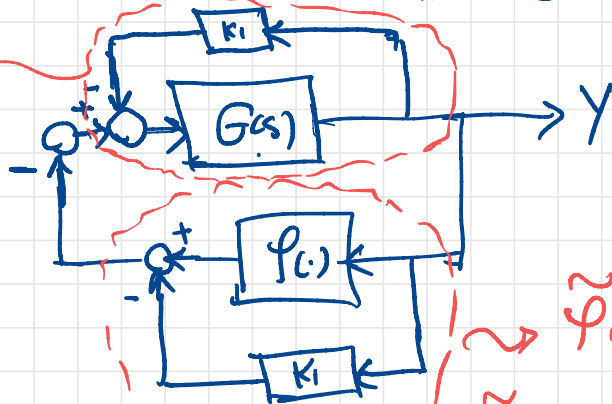
Back to absolute-stability: (circle criteria)

- Assume $\varphi \in [0, \infty]$
- Therefore φ is passive
- The FB sys. is stable if $G(s)$ is passive.
- Pictorially, the Nyquist plot is in the right-hand plane.



- Now, if $\varphi \in [K_1, \infty]$, we do a loop transformation to turn φ to $\tilde{\varphi} \in [0, \infty]$

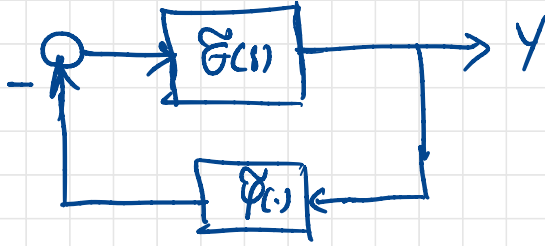
$$\tilde{G}(s) = \frac{G(s)}{1 + K_1 G(s)}$$



$$\tilde{\varphi}(y) = \varphi(y) - K_1 y$$

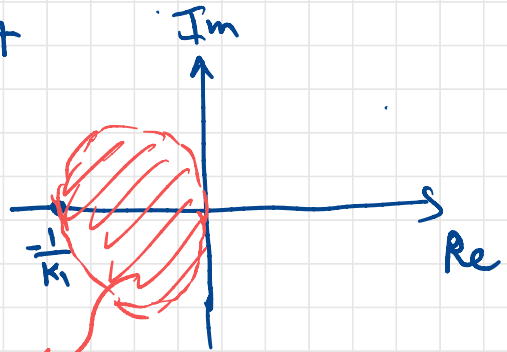
$$\tilde{\varphi}(y) = \varphi(y) - K_1 y$$

- Equivalent loop



- So, to have a passive FB sys. $\tilde{G}(s) = \frac{G(s)}{1+K_1G(s)}$ should be positive real

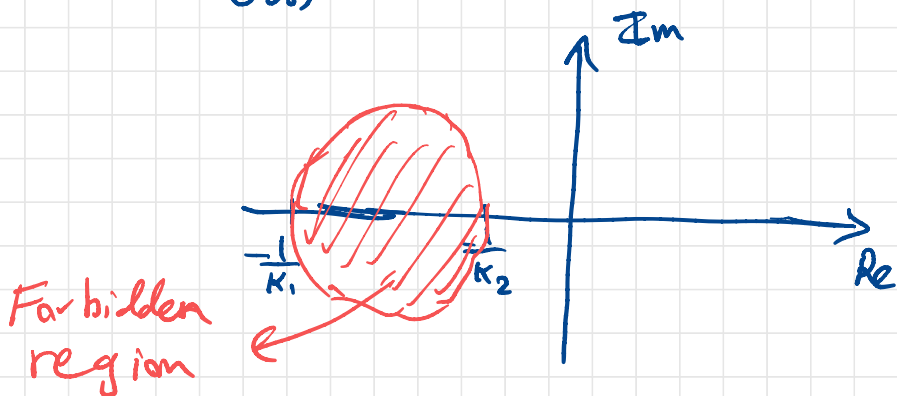
- Pictorially, in Nyquist plot



Forbidden region
(Circle criteria)

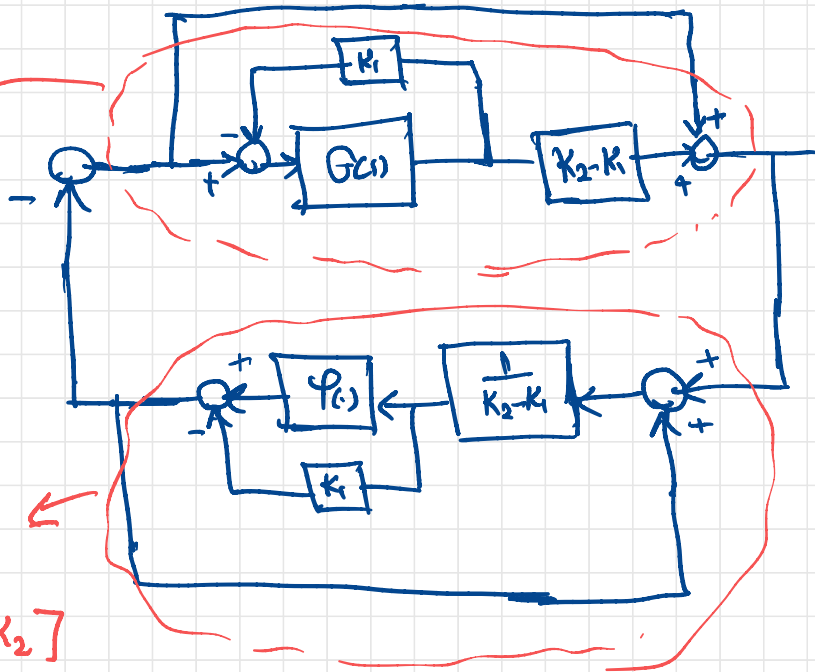
- More, generally, if $\varphi \in [K_1, K_2]$, then with loop transformation, we have

$$\tilde{G}(s) = \frac{1 + K_2 \Theta(s)}{1 + K_1 \Theta(s)} \quad \text{to be positive real.}$$



Loop trans.?

$$\tilde{G}(s) = \frac{1 + K_2 \Theta(s)}{1 + K_1 \Theta(s)}$$



$\tilde{\varphi} \in [0, \infty]$
when $\varphi \in [K_1, K_2]$